

Instabilité du usage de gaz incompressible

$$1 * \frac{\partial}{\partial t} (\rho_0 + \tilde{\rho}) + \text{div} [(\rho_0 + \tilde{\rho})(\vec{u} + \vec{u}_0)] = 0$$

$$\frac{\partial}{\partial t} \rho_0 + \rho_0 \text{div} \vec{u}_0 + \frac{\partial}{\partial t} \tilde{\rho} + \rho_0 \text{div} \vec{u} + \tilde{\rho} \text{div} \vec{u}_0 = 0$$

$$\text{or } \begin{matrix} \text{div} \vec{u}_0 = 0 \\ \vec{u}_0 = 0 \end{matrix} \Rightarrow \frac{\partial}{\partial t} \tilde{\rho} + \rho_0 \text{div} \vec{u} + \tilde{\rho} \text{div} \vec{u}_0 = 0$$

$$* (\rho_0 + \tilde{\rho}) \left[\frac{\partial \vec{u}_0}{\partial t} + \frac{\partial \vec{u}}{\partial t} + (\vec{u}_0 \cdot \nabla) (\vec{u}_0 + \vec{u}) + (\vec{u} \cdot \nabla) (\vec{u}_0 + \vec{u}) \right]$$

$$= -\nabla \rho_0 - \nabla \tilde{\rho} - \rho_0 \nabla (\phi_0 + \phi) - \tilde{\rho} \nabla (\phi_0 + \tilde{\phi})$$

$$\rho_0 \left[\frac{\partial \vec{u}_0}{\partial t} + (\vec{u}_0 \cdot \nabla) \vec{u}_0 + (\vec{u}_0 \cdot \nabla) \vec{u} + (\vec{u} \cdot \nabla) \vec{u}_0 + (\vec{u} \cdot \nabla) \vec{u} \right] +$$

$$\tilde{\rho} \left[\frac{\partial \vec{u}_0}{\partial t} + (\vec{u}_0 \cdot \nabla) \vec{u}_0 + \frac{\partial \vec{u}}{\partial t} + (\vec{u}_0 \cdot \nabla) \vec{u} + (\vec{u} \cdot \nabla) \vec{u}_0 + (\vec{u} \cdot \nabla) \vec{u} \right]$$

$$= -\nabla \rho_0 - \nabla \tilde{\rho} - \rho_0 \nabla (\phi_0 + \phi) - \tilde{\rho} \nabla (\phi_0 + \tilde{\phi})$$

$$\frac{d\vec{a}}{dt} \tilde{\rho} \left[\frac{\partial \vec{u}}{\partial t} + (\vec{u}_0 \cdot \nabla) \vec{u} + (\vec{u} \cdot \nabla) \vec{u} \right] + \rho_0 \left[\frac{\partial \vec{u}}{\partial t} + (\vec{u}_0 \cdot \nabla) \vec{u} + (\vec{u} \cdot \nabla) \vec{u} \right]$$

$$= -\nabla \tilde{\rho} - \rho_0 \nabla \phi - \tilde{\rho} \nabla \phi_0 - \tilde{\rho} \nabla \tilde{\phi}$$

$$* \nabla^2 \phi_0 + \nabla^2 \tilde{\phi} = 4\pi G (\rho_0 + \tilde{\rho}) \Leftrightarrow \nabla^2 \tilde{\phi} = 4\pi G \tilde{\rho}$$

$$* \rho_0 + \tilde{\rho} = c_s^2 (\rho_0 + \tilde{\rho}) \Leftrightarrow \tilde{\rho} = c_s^2 \tilde{\rho}$$

2. linearisation

$$* \frac{\partial}{\partial t} \tilde{\rho} + \rho_0 \text{div} \vec{u} = 0 \quad (1)$$

$$* \rho_0 \frac{\partial \vec{u}}{\partial t} = -\nabla \tilde{\rho} - \rho_0 \nabla \tilde{\phi} \quad (2)$$

$$* \nabla^2 \tilde{\phi} = 4\pi G \tilde{\rho} \quad (3)$$

$$* \tilde{\rho} = c_s^2 \tilde{\rho} \quad (4)$$

3- on prend la divergence de l'équation (2)

$$\operatorname{div} \left[\rho_0 \frac{\partial \vec{u}}{\partial t} \right] = - \operatorname{div} \vec{g} + \rho_0 \operatorname{div} \vec{g} = \rho_0 \operatorname{div} \vec{g}$$

$$\left. \begin{aligned} \text{ou } \frac{\partial \rho_0}{\partial t} = 0 \Rightarrow \operatorname{div} \rho_0 \frac{\partial \vec{u}}{\partial t} &= \frac{\partial}{\partial t} \operatorname{div} [\rho_0 \vec{u}] \\ \text{ou } \operatorname{div} \rho_0 \vec{u} &= - \frac{\partial \rho}{\partial t} \quad \text{eq (1)} \end{aligned} \right\} \operatorname{div} \rho_0 \frac{\partial \vec{u}}{\partial t} = - \frac{\partial^2 \rho}{\partial t^2}$$

d'où

$$- \frac{\partial^2 \rho}{\partial t^2} + \nabla^2 \rho + \rho_0 \nabla^2 \phi = 0$$

enfin $\nabla^2 \phi = 4\pi G \rho$ et $\rho = \frac{1}{c_s^2} \tilde{P}$ ou a

$$- \frac{1}{c_s^2} \frac{\partial^2 \tilde{P}}{\partial t^2} + \nabla^2 \tilde{P} + \rho_0 \frac{4\pi G}{c_s^2} \tilde{P} = 0$$

$$\boxed{- \frac{\partial^2 \tilde{P}}{\partial t^2} + c_s^2 \nabla^2 \tilde{P} + \rho_0 4\pi G \tilde{P} = 0}$$

$$\tilde{P} = P e^{i(\vec{k} \cdot \vec{r} - \omega t)}$$

$$\frac{\partial^2 \tilde{P}}{\partial t^2} = -\omega^2 \tilde{P} \quad \nabla^2 \tilde{P} = -k^2 \tilde{P}$$

soit $+\omega^2 P - c_s^2 k^2 P + \rho_0 4\pi G P = 0$

4- $\boxed{+\omega^2 = c_s^2 k^2 - 4\pi \rho_0 G}$

5- $k^2 = \frac{4\pi \rho_0 G}{c_s^2} + \frac{\omega^2}{c_s^2} \Rightarrow k = \frac{\omega}{c_s} \sqrt{1 + \frac{4\pi \rho_0 G c_s^2}{\omega^2}}$

$$\omega^2 = c_s^2 k^2 - 4\pi \rho_0 G$$

$$\omega = \pm \sqrt{c_s^2 k^2 - 4\pi \rho_0 G}$$

d'où $\boxed{k_c^2 = \frac{4\pi \rho_0 G}{c_s^2}}$

II Sillage turbulent d'un objet propulsé

- 1) la contrainte visqueuse, $\sigma'_{xy} = \eta \frac{\partial \bar{u}}{\partial y}$, s'annule à chaque extremum de \bar{u} en $y=0$ et en $y = \pm y_{\min}(\bar{u})$.
 la contrainte turbulente, $\bar{u}_{xy} = -\rho \overline{u'v'}$, change de signe en $y=0$ par symétrie.

$$2) \frac{\partial \bar{u}}{\partial t} + \bar{u} \frac{\partial \bar{u}}{\partial x} + \bar{v} \frac{\partial \bar{u}}{\partial y} = -\frac{1}{\rho} \frac{\partial \bar{p}}{\partial x} - \frac{\partial \overline{u'^2}}{\partial x} - \frac{\partial \overline{u'v'}}{\partial y} + \nu \left(\frac{\partial^2 \bar{u}}{\partial x^2} + \frac{\partial^2 \bar{u}}{\partial y^2} \right)$$

$$\frac{\partial \bar{v}}{\partial t} + \bar{u} \frac{\partial \bar{v}}{\partial x} + \bar{v} \frac{\partial \bar{v}}{\partial y} = -\frac{1}{\rho} \frac{\partial \bar{p}}{\partial y} - \frac{\partial \overline{u'v'}}{\partial x} - \frac{\partial \overline{v'^2}}{\partial y} + \nu \left(\frac{\partial^2 \bar{v}}{\partial x^2} + \frac{\partial^2 \bar{v}}{\partial y^2} \right)$$

- 3) L'éq. de Reynolds projetée selon y se réduit à $\frac{\partial \bar{p}}{\partial x} = -\rho \frac{\partial \overline{v'^2}}{\partial y}$
 ssi • écoulement statistiq. stationnaire $\frac{\partial \bar{v}}{\partial t} = 0$

- viscosité négligeable $\nu = 0$.
- $\left\| \frac{\partial \overline{u'v'}}{\partial x} \right\| \ll \left\| \frac{\partial \overline{v'^2}}{\partial y} \right\|$ car $l(x) \ll x$.
- $\frac{\partial \bar{u}}{\partial x} + \frac{\partial \bar{v}}{\partial y} = 0 \Rightarrow \bar{v} \approx \frac{l(x)}{x} U_s$.
- O.g. $\left(\bar{u} \frac{\partial \bar{v}}{\partial x} \right) = U_0 U_s \frac{l(x)}{x^2} \gg$ O.g. $\left(\bar{v} \frac{\partial \bar{v}}{\partial y} \right) = \frac{U_s^2 l(x)}{x}$
- O.g. $\left(\bar{u} \frac{\partial \bar{v}}{\partial x} \right) = U_0 U_s \frac{l(x)}{x^2} \ll$ O.g. $\left(\frac{\partial \overline{v'^2}}{\partial y} \right) = \frac{u_*'^2}{l(x)}$

ssi $\boxed{\left(\frac{l}{x} \right)^2 \frac{U_0 U_s}{u_*'^2} \ll 1}$

DS ce cas $\frac{\partial \bar{p}}{\partial x} = -\rho \frac{\partial \overline{v'^2}}{\partial y}$ et, en intégrant, on trouve que
 $\bar{p}(y) = p_0 - \rho \overline{v'^2}(y) + f(x)$
 $= 0$ car $\bar{p} = 0$ à l_0 .

4) L'éq. de Reynolds selon x :

$$\bullet -\frac{1}{\rho} \frac{\partial \bar{p}}{\partial x} = \frac{\partial \bar{v}^2}{\partial x} \ll \frac{\partial \bar{u} \bar{v}}{\partial y}$$

$$\bullet \text{O.g.} : \left(\bar{u} \frac{\partial \bar{u}}{\partial x} \right) = \frac{U_0 U_s}{x} \gg \text{O.g.} \left(\bar{v} \frac{\partial \bar{u}}{\partial y} \right) = \frac{U_s^2}{x}$$

$$\bullet \bar{u} \frac{\partial \bar{u}}{\partial x} = (U_0 - \Delta U) \frac{\partial (U_0 - \Delta U)}{\partial x} = -(U_0 - \Delta U) \frac{\partial \Delta U}{\partial x} \approx -U_0 \frac{\partial \Delta U}{\partial x}$$

Enfin, on obtient :

$$\boxed{U_0 \frac{\partial \Delta U}{\partial x} = \frac{\partial \bar{u} \bar{v}}{\partial y}}$$

$$5) \int_{-\infty}^{+\infty} U_0 y^2 \frac{\partial \Delta U}{\partial x} dy = - \int_{-\infty}^{+\infty} \nu_T(x) y^2 \frac{\partial^2 \bar{u}}{\partial y^2} dy$$

$$U_0 \frac{\partial}{\partial x} \int_{-\infty}^{+\infty} y^2 \Delta U dy = \nu_T(x) \int_{-\infty}^{+\infty} y^2 \frac{\partial^2 \Delta U}{\partial y^2} dy$$

on intègre par parties : $u = y^2$ et $v' = \frac{\partial^2 \Delta U}{\partial y^2}$

$$= \nu_T(x) \left\{ \underbrace{\left[y^2 \frac{\partial \Delta U}{\partial y} \right]_{-\infty}^{+\infty}}_0 - \int_{-\infty}^{+\infty} 2y \frac{\partial \Delta U}{\partial y} dy \right\}$$

puis $u = y$ et $v' = \frac{\partial \Delta U}{\partial y}$

$$= -2\nu_T(x) \left\{ \underbrace{\left[y \Delta U \right]_{-\infty}^{+\infty}}_0 - \int_{-\infty}^{+\infty} \Delta U dy \right\} = 0$$

$\Rightarrow I = \int_{-\infty}^{+\infty} y^2 \Delta U(x, y) dy$ est indpt de x .

$$6) \Delta U(x, y) = U_s(x) f(\zeta) \quad \text{où } f \text{ est paire et } \begin{cases} f(0) = 1 \\ f(\pm 1) = 0 \text{ et } f(\pm \infty) = 0 \end{cases}$$

$$I = \int_{-\infty}^{+\infty} y^2 \Delta U dy = f^3(x) U_s(x) \int_{-\infty}^{+\infty} \zeta^2 f(\zeta) d\zeta$$

soit $f^3(x) U_s(x) = J = \frac{I}{\int_{-\infty}^{+\infty} \zeta^2 f(\zeta) d\zeta}$

$$\Rightarrow 3l^2(x) U_s(x) \frac{dl}{dx} + l^3 \frac{dU_s}{dx} = 0 \Rightarrow \boxed{\frac{dU_s}{dx} = -3 \frac{U_s(x)}{l(x)} \frac{dl}{dx}}$$

7) $H_T(x) = \nu l(x) U_s(x)$ est le produit de la taille des structures turbulentes par leur vit. caractéristique.

$$8) \frac{\partial}{\partial y} = \frac{1}{l(x)} \frac{\partial}{\partial \zeta} \quad \text{et} \quad \frac{\partial}{\partial x} = -\frac{1}{l(x)} \frac{dl}{dx} \zeta \frac{\partial}{\partial \zeta}$$

$$U_0 \frac{dU_s}{dx} f(\zeta) - \frac{U_0 U_s}{l} \frac{dl}{dx} \zeta f' = \nu \frac{U_s^2}{l} f''$$

on obtient finalement :

$$\boxed{\frac{-f''}{3f + \zeta f'} = -\frac{U_0}{\nu} \frac{1}{U_s(x)} \frac{dl}{dx} = d} \quad (*)$$

$$9) \left. \begin{array}{l} \frac{1}{U_s(x)} \frac{dl}{dx} = d \Rightarrow \boxed{m = n + 1} \\ f^3(x) U_s(x) = c \frac{U_s^2}{l} \Rightarrow \boxed{n = -3m} \end{array} \right\} \Rightarrow \boxed{\begin{array}{l} m = 1/4 \\ n = -3/4 \end{array}} \quad \begin{array}{l} U_s(x) \propto x^{-3/4} \\ l(x) \propto x^{1/4} \end{array}$$

$Re_T(x) = \frac{U_s(x) l(x)}{\nu} \propto x^{-1/2} \Rightarrow$ retour au laminaire loin derrière l'objet, contrairement au sillage d'un objet passif.

$H_T(x) \propto x^{-1/2} \Rightarrow$ la contrainte turbulente disparaît loin de l'objet \Rightarrow retour au laminaire.

10) On s'attend à ce que $H_T = 0$ loin de l'axe $y \gg l(x)$.
 Il aurait fallu tenir compte d'une décroissance de H_T avec y pour que notre modèle soit pertinent.
 Ce modèle est adapté proche du centre en $y \approx 0$ et marche moins bien loin du centre $y \gg l(x)$.

$$11) f'' + 3f + \zeta f' = 0 \quad \text{d'après (*) si } d=1$$

$$f(\zeta) = \frac{\partial^2}{\partial \zeta^2} \left[\exp\left(-\frac{1}{2}\zeta^2\right) \right] = (\zeta^2 - 1) \exp\left(-\frac{1}{2}\zeta^2\right)$$

$$f'(z) = (3z - z^3) \exp\left(-\frac{1}{2}z^2\right)$$

$$f''(z) = (3 - 6z^2 + z^4) \exp\left(-\frac{1}{2}z^2\right)$$

on injecte ds $f'' + 3f + z f' = 0$ et se vérifie. $f(z)$ est bien solution.

on vérifie que $f(\pm\infty) = f(\pm 1) = 0$

$$f(0) = -1 \Rightarrow \bar{u}(x, 0) = U_0 - \Delta U(x, 0) \\ = U_0 - U_s(x) f(0) = U_0 + U_s$$

$$12) -\bar{u}_{,yy} = g(z) U_s^2(x) = \mu_T(x) \frac{\partial \bar{u}}{\partial y}$$

$$\mu_T(x) U_s^2(x) \frac{1}{U_s^2(x)} U_s^2(x) f' = U_s^2(x) g$$

$$\Rightarrow \boxed{g = \mu f'} \quad g \text{ est impaire}$$

$$\text{et } g(z) = (3z - z^3) \exp\left(-\frac{1}{2}z^2\right)$$